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Mechanically robust stretchable organic optoelectronic devices built using a simple and universal stencil-pattern transferring technology

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Abstract

Stretchable electronic and optoelectronic devices based on controllable ordered buckling structures exhibit superior mechanical stability by retaining their buckling profile without distortion in repeated stretch-release cycles. However, a simple and universal technology to introduce ordered buckling structures into stretchable devices remains a real challenge. Here, a simple and general stencil-pattern transferring technology was applied to stretchable organic light-emitting devices (SOLEDs) and polymer solar cells (SPSCs) to realize an ordered buckling profile. To the best of our knowledge, both the SOLEDs and SPSCs with periodic buckles exhibited the highest mechanical robustness by operating with small performance variations after 20000 and 12000 stretch-release cycles between 0% and 20% tensile strain, respectively. Notably, in this work, periodic buckled structures were introduced into SPSCs for the first time, with the number of stretch-release cycles for the SPSCs improved by two

orders of magnitude compared to that for previously reported random-buckled stretchable organic solar cells. The simple method used in this work provides a universal solution for low-cost and high-performance stretchable electronic and optoelectronic devices and promotes the commercial development of stretchable devices in wearable electronics.

Keywords: organic light-emitting devices, periodic buckles, polymer solar cells, stencil-pattern transferring process, stretchable

INTRODUCTION

Stretchable electronic and optoelectronic devices such as stretchable light-emitting devices¹⁻⁷, solar cells⁸⁻¹¹, supercapacitors¹²⁻¹⁵, batteries¹⁶⁻¹⁸, conductors¹⁹⁻²³ and sensors²⁴⁻²⁷ show great potential for next-generation wearable electronics applications. Among various strategies to realize stretchable devices²⁸⁻³³, the creation of a buckling profile in ultrathin devices has attracted much attention because of its independence from materials and the structures of these devices, enabling flexibility for device fabrication³⁴⁻⁴³. Different types of buckled ultrathin film-based stretchable electronic and optoelectronic devices have been reported. The process for forming the buckles determines the morphology for ultrathin films and is important for the performance of stretchable devices. Random buckles can be formed by attaching an ultrathin film onto a pre-strained adhesive and elastomeric substrate, followed by the release of the substrate without any control^{34, 36, 39, 40, 42}. Small-bending radii in sharp corners and extreme-bending regions result in a large-bending strain, which can damage devices. Additionally, the profile of random buckles might change after cyclic stretching due to the changing random bonding regions between ultrathin devices and the elastomeric substrate. Poor mechanical stability is a fatal disadvantage for random buckling stretchable devices due to the above factors. In contrast, devices based on controllable ordered buckles prepared via sophisticated configuration design and processing can avoid the formation of sharp corners and extreme bending and maintain the ordered buckling profile without distortion, which can much improve their mechanical stability. Introducing well-designed ordered structures on the surface of an adhesive and elastomeric substrate via the use of a programmable laser ablation process has been demonstrated as a feasible strategy to fabricate periodic buckles for stretchable organic light-emitting devices (SOLEDs) with high mechanical stability⁴¹. However, considering that the laser ablation system and process is both expensive and complicated, a simple and low-cost technology for realizing stretchable devices

with ordered buckles remains a real challenge, which is a major obstacle for the practical applications of stretchable devices.

The stencil-pattern transferring technique is commonly used for copying and transferring patterns to target substrates⁴⁴⁻⁵⁰. The dimension and size of the fabricated microstructures are the same as the patterns on the stencil. Deposited films with defined patterns can be directly utilized as functional layers, such as patterned metal electrodes in organic optoelectronic devices⁵¹⁻⁵⁶. Here, we developed a simple and general stencil-pattern transferring technique for fabricating ordered buckles in stretchable organic optoelectronic devices. A periodic metal film was deposited onto the surface of an adhesive and elastomeric substrate via a stencil and used as a barrier layer to modify the surface viscosity distribution of the substrate without affecting its elasticity. When an ultrathin optoelectronic device was attached onto the pre-stretched substrate, bonding and nonbonding regions between the device and substrate were defined by the periodic barrier layer. Controllable and ordered buckles have been achieved after releasing the pre-strained substrate. Stretchable organic light-emitting devices (SOLEDs) and polymer solar cells (SPSCs) were fabricated by a simple process. Notably, the SPSCs in this work are the first reported SPSCs with periodic buckled structures. The SOLEDs and SPSCs exhibited outstanding mechanical stability with small performance variations after 20000 and 12000 stretch-release cycles between 0% and 20% tensile strain, respectively. The periodic-buckled SPSCs exhibited enhancements of two orders of magnitude in the number of stretch-release cycles compared to that for previously reported random-buckled SPSCs^{11, 34, 43}. The simple and low-cost stencil-pattern transferring technique employed in this work exhibits great potential as a universal solution for various stretchable electronic and optoelectronic devices because of its compatibility with various materials, structures and fabrication processes for device fabrication; this compatibility is important for promoting the commercial development of stretchable electronic and optoelectronic devices in wearable electronics.

MATERIALS AND METHODS

Materials

Polymer substrates for ultrathin OLEDs and PSCs were fabricated by a NOA 63 photoresist, which was purchased from Norland Products Inc. (USA). Adhesive and elastomeric substrates (3M VHB 4905 tape) and plastic tapes (Scotch Magic Tape) were purchased from the 3M Company (USA). Metal stencils were custom-made by ZLDSK Corporation (China). MoO_3 , NPB (N,N'-diphenyl-N,N'-bis(1,1'-biphenyl)-4,4'-diamine), CBP (4,4'-bis(N-carbazolyl)-1,1'-biphenyl), $\text{Ir}(\text{BT})_2(\text{acac})$ (2,3,5,6-tetrakis(3,6-diphenylcarbazol-9-yl)-1,4-dicyanobenzene), TPBi (1,3,5-tris(N-phenyl-benzimidazol-2-yl)benzene), PCDTBT (poly(N-9'-heptadecanyl-2,7-carbazole-alt-5,5-(4',7-di-2-thienyl-2',1',3'-benzothiadiazole))) and PC_{71}BM ((6,6)-Phenyl C71 butyric acid methyl ester) were purchased from Luminescence Technology Corporation (Taiwan, China). Ca was purchased from Sigma-Aldrich (USA). Ag was purchased from ZhongNuo Advanced Material (Beijing, China) Technology Co., Ltd. All materials for the fabrication of the OLEDs and OPVs were used as received without any treatment.

Barrier layer fabrication

The adhesive and elastomeric substrate was cut to the desired size (5 cm \times 5 cm), and a working region (0.6 cm \times 5 cm) was defined by plastic tape. A metal stencil was attached onto the working region with the long axes parallel to each other. A layer of aluminum (Al) film was deposited onto the surface of the elastomeric substrate via the metal stencil by thermal evaporation (Fig. 1a). The thickness of the Al barrier layer was 50 nm. Then, the metal stencil was removed from the substrate and a periodic Al film was obtained as a barrier layer (Fig. 1b). The regions of the adhesive and elastomeric substrate covered by the Al film

lost viscosity. As shown in Fig. 1c, the substrate was pre-stretched, with the period of the Al barrier layer increased.

SOLEDs fabrication

Ultrathin OLEDs were fabricated by a stripping process⁴⁰. An Ir(BT)₂(acac) doped CBP film was used as the emitting layer. The detailed device structure was Ag/MoO₃/NPB/CBP:Ir(BT)₂(acac)/TPBi/Ca/Ag, as shown in Supplementary Fig. S1. The free-standing ultrathin OLED was placed onto the surface of a roller and then transferred to the pre-stretched elastomeric substrate (Fig. 1d). During this process, bonding was limited to only the bare regions of the substrate, with no bonding occurring at the Al barrier layer regions. Finally, in Figure 1e, SOLEDs with periodic buckles were formed after releasing the pre-stretched elastomeric substrate. The original length of the elastomeric substrate was 6 mm, which was increased to 18 mm after stretching to 200% strain. During the buckle forming process shown in Fig. 1d to Fig. 1e, the length of the elastomeric substrate contracted to 9 mm. When re-stretching the devices, the largest tensile strain was 100% according to the length increase from 9 mm to 18 mm.

For the fabrication process of the SOLED array, the stencil used for Al barrier layer deposition contained a period of 550 μm , of which the width of the open spaces and metal lines were 450 μm and 100 μm , respectively, as shown in Supplementary Fig. S2. OLED stripes were precisely attached onto the adhesive bare regions of the adhesive to ensure overlap for the period of the OLED array and the Al barrier layer.

Fabrication of SPSCs

Ultrathin PSCs were fabricated by the same stripping process as used for SOLEDs. NOA 63 film coated onto a silicon slice was first transferred into a vacuum chamber to thermally deposit an Ag cathode and TPBi layer. Then, a solution of PCDTBT:PC₇₁BM (1:4 w/w,

polymer concentration of 25 mg mL⁻¹ in 1,2-dichlorobenzene) was spin-coated atop the TPBi layer. The spin-coating speed was 3000 rpm for half a minute. The resulting film had a thickness of approximately 80 nm. The whole semi-finished device was annealed on a heating stage at 70 °C for 60 min in a glove box filled with inert gas. Finally, the sample was transferred into the vacuum chamber again to deposit the MoO₃, Au and Ag layers. The ultrathin polymer solar cell was peeled off from the silicon slice and attached onto the pre-stretched elastomeric substrate. SPSCs with periodic buckles were formed after releasing the substrate.

Characterization

All SEM images were taken by a JEOL JSM-7500F scanning electron microscope (JEOL Ltd.). An XP-2 stylus profilometer (Ambios Technology, Inc.) was utilized to measure the thickness of the ultrathin NOA63 film. I–L–V characteristics for all OLEDs were investigated by a Keithley 2400 source meter and a Photoresearch PR-655 spectrophotometer with an MS-75 and SL-1x composite lens. PSCs and SPSCs were characterized by a Keithley 2400 source meter under illumination provided by a solar simulator (AM 1.5 Global spectrum, with a light intensity of 100 mW cm⁻²).

RESULTS AND DISCUSSION

The metal stencil is shown in Supplementary Fig. S3. The period of the patterns is 400 μm, of which the widths of the open space and the metal line are 300 μm and 100 μm, respectively. As shown in Fig. 1a, the stencil seamlessly contacted with the adhesive and elastomeric substrate. As a result, the obtained Al barrier layer was uniform and showed the same period as the stencil pattern as shown in the scanning electron microscope (SEM) image in Fig. 1f. After stretching the substrate to 200% strain, the period of the Al barrier layer changed (Fig.

1g). In particular, its period increased to 1200 μm , of which the width of the metal stripe region and the bare region were approximately 900 μm and 300 μm , respectively. The increasing proportion was identical to the tensile strain, which demonstrated that the deposited thin Al film did not affect the stretchability of the elastomeric substrate. The uniform deformation of the elastomeric substrate was beneficial for ordered buckle formation. The inset of Fig. 1f shows the surface morphology of the thermally evaporated Al film for a zoomed-in region. A large roughness and masses of small random wrinkles can be observed. The morphology of the metal films deposited by thermal evaporation is related to the receiving substrate materials⁵⁷⁻⁵⁹. The Al film fractured to small fragments after being stretched to 200% strain (inset of Fig. 1g). The fracture phenomenon was also observed in Al films with different thicknesses, as shown in Supplementary Fig. S4. The width of the Al fragments and their gaps were all smaller than 10 μm with various thicknesses.

SOLEDs and SPSCs based on the stencil-pattern transferring process were fabricated. Ultrathin OLEDs and PSCs were obtained by fabricating devices on ultrathin polymer films. The total thickness of the ultrathin devices was approximately 3 μm , of which the polymer film thickness was approximately 2.8 μm . Figure 2 shows the SOLEDs at different tensile strain. The ultrathin OLEDs only adhered to the periodic bare regions and bent above the Al regions of the substrate, as shown in Fig. 2a. Periodic buckles within the whole ultrathin device were formed, which demonstrated effective control of the buckling process through the Al barrier layer. With 200% pre-strain, the SOLEDs exhibited a large tensile strain of 100%. The decreased stretchability was due to incomplete contracting of the elastomeric substrate. The compressive stress of the elastomeric substrate decreased gradually after releasing the pre-strain. At the same time, the small-bending radii resulted in a large-bending stress, with corresponding large resistance in the compressive direction, which hindered the elastomeric substrate from absolutely contracting to its original state. The period of the buckles was the

same as that of the Al films at various stretched states. At the largest applied tensile strain of 100%, the periodic buckles disappeared.

Figure 2b and Supplementary Movie 1 show the operating SOLEDs in static and dynamic states, respectively. Ir(BT)₂(acac) was used as the light-emitting material, with yellow emission realized. The bright light-emission area gradually elongated with increasing tensile strain, which visually showed the stretchability of the SOLEDs. Periodic buckles and the Al barrier layer can be clearly seen. The operation of the SOLEDs in a dark environment was also investigated, as shown in Fig. 3. Figure 3a shows a large-area SOLED containing nine periods of buckles at different strains. The visible periodic buckles slightly influence the uniformity of the emission observed from the SOLED. Figure 3b (Supplementary Movie 2) shows an array of five OLED pixels; this array forms a pattern of light and dark stripes. The period of the array was the same as that of the buckles. Periodic buckles formed at lower strain and light from each pixel was reflected by an adjacent non-planar metal anode film, which made each pixel look wider. The synchronization of the periodic buckles and the OLED array reveal the potential applications for the SOLED in stretchable displays.

The electroluminescence (EL) performance of the SOLEDs was measured at different stretched states, as shown in Fig. 4a and 4b. The EL performance of the SOLEDs was excellent, stable at different tensile strain and comparable to that of the planar device. The maximum current efficiency at 0% and 100% tensile strain was 71 cd A⁻¹ and 73 cd A⁻¹, respectively, with a variation of only 2.8%. Supplementary Fig. S5 shows the EL spectra measured at different strain values. A redshift in the spectral curves was observed with increasing tensile strain, which results from the microcavity effect in SOLEDs⁴¹. The slight redshift (approximately 5 nm) was in agreement with the stable current efficiency. The above results indicate that the periodic buckling profile introduced into the SOLEDs leads to negligible deterioration of the device performance.

The mechanical stability of the SOLEDs was examined by cyclically stretching the devices between varying strain values. The SOLED was measured at 0% strain after every 500 stretch-release cycles in air without any encapsulation. The driving voltage was 5.5 V. Figure 4c and 4d show the EL performance of the SOLEDs. The luminance increased by approximately 20% during the first 3000 cycles of cyclic stretching and became stable in the following test between 0% and 20% strain (Fig. 4c). Similarly, the luminance of SOLEDs slightly increased during cyclic stretching between 0% and 60% strain, as shown in Fig. 4d. The current efficiency exhibited a slight variation of 2%. As seen from Supplementary Fig. S6 and S7, the normalized current density for the SOLEDs under the cyclic stretching test showed a similar increase during the initial 3000 cycles. A possible origin for the increased current density for the initial 3000 stretch-release cycles is the compression effect in small-molecule semiconductor films, as shown in Supplementary Fig. S8.^{60, 61} The SOLED was found to be mechanically robust, as demonstrated by the cyclic stretching tests. The mechanical robustness was attributed to the ordered buckles. The Al films degraded little and maintained good adhesion with the elastomeric substrate after 20000 cycles of cyclic stretching (Supplementary Fig. S9). The SOLEDs retained an ordered buckling profile without distortion during the stretch-release process (Supplementary Fig. S10). Any defects in the device can be spread and amplified after thousands of stretch-release cycles, resulting in degraded performance. The smallest bending radius for the periodic buckles was approximately 100 μm at 0% strain, as shown in Fig. 2a. The bending strain determined by the bending radius and thickness of the ultrathin OLEDs was only approximately 0.68% for the metallic anode⁴⁰. Therefore, the bending deformation due to the periodic buckles did not cause obvious mechanical and electrical damage to the SOLEDs, and they could operate stably and efficiently with such large-bending strain during cyclic stretching.

Stretchable solar cells are an important member of stretchable organic optoelectronics. Efficient and mechanically robust stretchable solar cells are the best candidates for electric power suppliers in a stretchable electronic system integrated with other stretchable electronic devices. However, previously reported stretchable solar cells with random buckles could only withstand tens to hundreds of cyclic stretches, which hindered their use for commercial applications^{11, 34, 39, 43}. Here, we demonstrated mechanically robust SPSCs based on the use of a simple stencil-pattern transferring technology. This paper presents the first report of SPSCs with periodic buckling structures. The device structure of an ultrathin polymer solar cell is shown in Supplementary Fig. S11. A polymer-fullerene derivative PCDTBT:PC₇₁BM blend was used as light absorber. The SPSCs were also fabricated by following the steps shown in Fig. 1a-e. Periodic buckles were formed, with a large tensile strain of up to 100%, as shown in Supplementary Fig. S12. The J-V characteristic curve for a planar solar cell is shown in Fig. 5a. Its power conversion efficiency (PCE) was 5.1%, with an open-circuit voltage (V_{OC}) of 0.78 V, short-circuit current density (J_{SC}) of 12 mA cm⁻² and fill factors (FF) of 54%, which are comparable with the best reported polymer solar cells based on PCDTBT:PC₇₁BM^{62, 63}. The I-V characteristics for the SPSCs were measured for varying tensile strain values, as shown in Fig. 5b. The devices worked functionally at each stretched state. The normalized values for V_{OC} , I_{SC} , FF and output power at different tensile strain are summarized in Fig. 5c. The output power was defined as

$$\text{Output power} = V_{OC} \cdot I_{SC} \cdot FF \quad (1).$$

V_{OC} and FF changed little, while I_{SC} and the output power increased almost linearly with increasing tensile strain. This outcome was attributed to the increased light incident area, with tensile strain increasing despite the practical device area not changing. At the same time, the linearly increased I_{SC} indicated that the periodic buckles had nearly no influence on the light absorption in the SPSCs.

The mechanical stability of the SPSCs was examined by cyclically stretching the devices between 0% and 20% tensile strain, as shown in Fig. 5d. The I-V characteristics were measured at 0% strain after every 500 stretch-release cycles. The SPSCs could survive 12000 stretch-release cycles; this value is two orders of magnitude higher than that reported in previous results obtained for random-buckle-based SPSCs^{11, 34, 43}. To the best of our knowledge, our mechanical stability for SPSCs is the highest reported to date. It should be noted that the degradation in V_{OC} and FF was quite small. The stable FF indicated that no large damage due to cracks or delamination was introduced into the PSCs during the cycling, so as not to affect the conductivity and series resistance. The clearly fluctuant I_{SC} might be caused by the fluctuant incident area for the SPSCs at 0% strain under each measurement. The elastomeric substrate is visco-elastic. Thus, it would take some time to contract to 0% strain state absolutely, especially under continuously cyclic stretching. Therefore, a small variation exists in the incident area for each measurement during the cyclic stretching test, leading to the observed fluctuation in I_{SC} .

CONCLUSIONS

A simple and universal stencil-pattern transferring technology was applied to stretchable organic optoelectronic devices, resulting in the demonstration of high-performance SOLEDs and SPSCs with periodic buckles. A periodic Al barrier layer that was deposited onto elastomeric substrates by a stencil pattern played the role of forming periodic buckles for ultrathin optoelectronic devices. The SOLEDs and SPSCs both exhibited the highest mechanical robustness reported to date; notably, the SPSCs showed an improvement of two orders of magnitude. Stretchability, efficiency, mechanical stability and production cost are key factors for practical applications of stretchable optoelectronics. The simple and universal stencil-pattern transferring technology used in this work provides a solution for low-cost and

high-performance stretchable optoelectronic devices and demonstrates potential for commercial development of stretchable electronics and optoelectronics.

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REFERENCES

- 1 Bade SGR, Shan X, Hoang PT, Li JQ, Geske T *et al.* Stretchable light-emitting diodes with organometal-halide-perovskite-polymer composite emitters. *Adv Mater* 2017; **29**: 1607053.
- 2 Wang JX, Yan CY, Cai GF, Cui MQ, Lee-Sie Eh A *et al.* Extremely stretchable electroluminescent devices with ionic conductors. *Adv Mater* 2016; **28**: 4490-4496.
- 3 Larson C, Peele B, Li S, Robinson S, Totaro M *et al.* Highly stretchable electroluminescent skin for optical signaling and tactile sensing. *Science* 2016; **351**: 1071-1074.
- 4 Liang JJ, Li L, Niu XF, Yu ZB, Pei QB. Elastomeric polymer light-emitting devices and displays. *Nat Photonics* 2013; **7**: 817-824.
- 5 Jeong GS, Baek DH, Jung HC, Song JH, Moon JH *et al.* Solderable and electroplatable flexible electronic circuit on a porous stretchable elastomer. *Nat Commun* 2012; **3**: 977.
- 6 Hu XL, Krull P, de Graff B, Dowling K, Rogers JA *et al.* Stretchable inorganic-semiconductor electronic systems. *Adv Mater* 2011; **23**: 2933-2936.
- 7 Sekitani T, Nakajima H, Maeda H, Fukushima T, Aida T *et al.* Stretchable active-matrix organic light-emitting diode display using printable elastic conductors. *Nat Mater* 2009; **8**: 494-499.
- 8 Zhang ZT, Yang ZB, Deng J, Zhang Y, Guan GZ *et al.* Stretchable polymer solar cell fibers. *Small* 2015; **11**: 675-680.

- 9 O'Connor TF, Zaretski AV, Shiravi BA, Savagatrup S, Printz AD *et al.* Stretching and conformal bonding of organic solar cells to hemispherical surfaces. *Energy Environ Sci* 2014; **7**: 370-378.
- 10 Lipomi DJ, Chong H, Vosgueritchian M, Mei JG, Bao ZN. Toward mechanically robust and intrinsically stretchable organic solar cells: evolution of photovoltaic properties with tensile strain. *Sol Energy Mater Sol Cells* 2012; **107**: 355-365.
- 11 Lipomi DJ, Tee BCK, Vosgueritchian M, Bao ZN. Stretchable organic solar cells. *Adv Mater* 2011; **23**: 1771-1775.
- 12 Luan PS, Zhang N, Zhou WY, Niu ZQ, Zhang Q *et al.* Epidermal supercapacitor with high performance. *Adv Funct Mater* 2016; **26**: 8178-8184.
- 13 Choi C, Kim JH, Sim HJ, Di JT, Baughman RH *et al.* Microscopically buckled and macroscopically coiled fibers for ultra-stretchable supercapacitors. *Adv Energy Mater* 2017; **7**: 1602021.
- 14 Zhang QC, Sun J, Pan ZH, Zhang J, Zhao JX *et al.* Stretchable fiber-shaped asymmetric supercapacitors with ultrahigh energy density. *Nano Energy* 2017; **39**: 219-228.
- 15 Zhang ZT, Wang L, Li YM, Wang YH, Zhang J *et al.* Nitrogen-doped core-sheath carbon nanotube array for highly stretchable supercapacitor. *Adv Energy Mater* 2017; **7**: 1601814.
- 16 Zamarayeva AM, Ostfeld AE, Wang M, Dreyer JK, Deckman I *et al.* Flexible and stretchable power sources for wearable electronics. *Sci Adv* 2017; **3**: e1602051.
- 17 Kumar R, Shin J, Yin L, You JM, Meng YS *et al.* All-printed, stretchable Zn-Ag₂O rechargeable battery via hyperelastic binder for self-powering wearable electronics. *Adv Energy Mater* 2017; **7**: 1602096.
- 18 Li HS, Ding Y, Ha H, Shi Y, Peng LL *et al.* An all-stretchable-component sodium-ion full battery. *Adv Mater* 2017; **29**: 1700898.
- 19 Wang Y, Zhu CX, Pfattner R, Yan HP, Jin LH *et al.* A highly stretchable, transparent, and conductive polymer. *Sci Adv* 2017; **3**: e1602076.

- 20 Matsuhisa N, Inoue D, Zalar P, Jin H, Matsuba Y *et al.* Printable elastic conductors by in situ formation of silver nanoparticles from silver flakes. *Nat Mater* 2017; **16**: 834-840.
- 21 Cao Y, Morrissey TG, Acome E, Allec SI, Wong BM *et al.* A transparent, self-healing, highly stretchable ionic conductor. *Adv Mater* 2017; **29**: 1605099.
- 22 Jin H, Matsuhisa N, Lee S, Abbas M, Yokota T *et al.* Enhancing the performance of stretchable conductors for E-textiles by controlled ink permeation. *Adv Mater* 2017; **29**: 1605848.
- 23 Liu ZY, Wang XT, Qi DP, Xu C, Yu JC *et al.* High-adhesion stretchable electrodes based on nanopile interlocking. *Adv Mater* 2017; **29**: 1603382.
- 24 Cai YC, Shen J, Dai ZY, Zang XX, Dong QC *et al.* Extraordinarily stretchable all-carbon collaborative nanoarchitectures for epidermal sensors. *Adv Mater* 2017; **29**: 1606411.
- 25 Guo SZ, Qiu KY, Meng FB, Park SH, McAlpine MC. 3D printed stretchable tactile sensors. *Adv Mater* 2017; **29**: 1701218.
- 26 Ho MD, Ling YZ, Yap LW, Wang Y, Dong DS *et al.* Percolating network of ultrathin gold nanowires and silver nanowires toward “invisible” wearable sensors for detecting emotional expression and apexcardiogram. *Adv Funct Mater* 2017; **27**: 1700845.
- 27 Yamamoto Y, Yamamoto D, Takada M, Naito H, Arie T *et al.* Efficient skin temperature sensor and stable gel-less sticky ECG sensor for a wearable flexible healthcare patch. *Adv Healthc Mater* 2017; **6**: 1700495.
- 28 Kim DH, Rogers JA. Stretchable electronics: materials strategies and devices. *Adv Mater* 2008; **20**: 4887-4892.
- 29 Rogers JA, Someya T, Huang YG. Materials and mechanics for stretchable electronics. *Science* 2010; **327**: 1603-1607.
- 30 Lipomi DJ, Bao ZN. Stretchable, elastic materials and devices for solar energy conversion. *Energy Environ Sci* 2011; **4**: 3314-3328.

- 31 Chortos A, Liu J, Bao ZN. Pursuing prosthetic electronic skin. *Nat Mater* 2016; **15**: 937-950.
- 32 Qian Y, Zhang XW, Xie LH, Qi DP, Chandran BK *et al.* Stretchable organic semiconductor devices. *Adv Mater* 2016; **28**: 9243-9265.
- 33 Liu W, Song MS, Kong B, Cui Y. Flexible and stretchable energy storage: recent advances and future perspectives. *Adv Mater* 2017; **29**: 1603436.
- 34 Kaltenbrunner M, White MS, Glowacki ED, Sekitani T, Someya T *et al.* Ultrathin and lightweight organic solar cells with high flexibility. *Nat Commun* 2012; **3**: 770.
- 35 Kaltenbrunner M, Sekitani T, Reeder J, Yokota T, Kuribara K *et al.* An ultra-lightweight design for imperceptible plastic electronics. *Nature* 2013; **499**: 458-463.
- 36 White MS, Kaltenbrunner M, Glowacki ED, Gutnichenko K, Kettlgruber G *et al.* Ultrathin, highly flexible and stretchable PLEDs. *Nat Photonics* 2013; **7**: 811-816.
- 37 Fukuda K, Takeda Y, Yoshimura Y, Shiwaku R, Tran LT *et al.* Fully-printed high-performance organic thin-film transistors and circuitry on one-micron-thick polymer films. *Nat Commun* 2014; **5**: 4147.
- 38 Choi MK, Yang J, Kang K, Kim DC, Choi C *et al.* Wearable red-green-blue quantum dot light-emitting diode array using high-resolution intaglio transfer printing. *Nat Commun* 2015; **6**: 7149.
- 39 Kaltenbrunner M, Adam G, Glowacki ED, Drack M, Schwödiauer R *et al.* Flexible high power-per-weight perovskite solar cells with chromium oxide-metal contacts for improved stability in air. *Nat Mater* 2015; **14**: 1032-1039.
- 40 Yin D, Feng J, Jiang NR, Ma R, Liu YF *et al.* Two-dimensional stretchable organic light-emitting devices with high efficiency. *ACS Appl Mater Interfaces* 2016; **8**: 31166-31171.
- 41 Yin D, Feng J, Ma R, Liu YF, Zhang YL *et al.* Efficient and mechanically robust stretchable organic light-emitting devices by a laser-programmable buckling process. *Nat Commun* 2016; **7**: 11573.

- 42 Yokota T, Zalar P, Kaltenbrunner M, Jinno H, Matsuhisa N *et al.* Ultraflexible organic photonic skin. *Sci Adv* 2016; **2**: e1501856.
- 43 Ma R, Feng J, Yin D, Sun HB. Highly efficient and mechanically robust stretchable polymer solar cells with random buckling. *Org Electron* 2017; **43**: 77-81.
- 44 Deshmukh MM, Ralph DC, Thomas M, Silcox J. Nanofabrication using a stencil mask. *Appl Phys Lett* 1999; **75**: 1631-1633.
- 45 Brugger J, Berenschot JW, Kuiper S, Nijdam W, Otter B *et al.* Resistless patterning of sub-micron structures by evaporation through nanostencils. *Microelectron Eng* 2000; **53**: 403-405.
- 46 Kim GM, van den Boogaart MAF, Brugger J. Fabrication and application of a full wafer size micro/nanostencil for multiple length-scale surface patterning. *Microelectron Eng* 2003; **67-68**: 609-614.
- 47 Ye YH, Jeong DY, Zhang QM. Fabrication of strain tunable infrared frequency selective surfaces on electrostrictive poly(vinylidene fluoride-trifluoroethylene) copolymer films using a stencil mask method. *Appl Phys Lett* 2004; **85**: 654-656.
- 48 Lishchynska M, Bourenkov V, van den Boogaart MAF, Doeswijk L, Brugger J *et al.* Predicting mask distortion, clogging and pattern transfer for stencil lithography. *Microelectron Eng* 2007; **84**: 42-53.
- 49 Braam K, Subramanian V. A stencil printed, high energy density silver oxide battery using a novel photopolymerizable poly(acrylic acid) separator. *Adv Mater* 2015; **27**: 689-694.
- 50 Hyun WJ, Lim S, Ahn BY, Lewis JA, Frisbie CD *et al.* Screen printing of highly loaded silver inks on plastic substrates using silicon stencils. *ACS Appl Mater Interfaces* 2015; **7**: 12619-12624.
- 51 Liu BQ, Wang L, Gao DY, Zou JH, Ning HL *et al.* Extremely high-efficiency and ultrasimplified hybrid white organic light-emitting diodes exploiting double multifunctional blue emitting layers. *Light: Sci Appl* 2016; **5**: e16137.

- 52 Xu LH, Ou QD, LI YQ, Zhang YB, Zhao XD *et al.* Microcavity-free broadband light outcoupling enhancement in flexible organic light-emitting diodes with nanostructured transparent metal-dielectric composite electrodes. *ACS Nano* 2016; **10**: 1625-1632.
- 53 Liu YF, Feng J, Yin D, Bi YG, Song JF *et al.* Highly flexible and efficient top-emitting organic light-emitting devices with ultrasmooth Ag anode. *Opt Lett* 2012; **37**: 1796-1798.
- 54 Liu YF, Feng J, Cui HF, Zhang YF, Yin D *et al.* Fabrication and characterization of Ag film with sub-nanometer surface roughness as a flexible cathode for inverted top-emitting organic light-emitting devices. *Nanoscale* 2013; **5**: 10811-10815.
- 55 Guo F, Karl A, Xue QF, Tam KC, Forberich K *et al.* The fabrication of color-tunable organic light-emitting diode displays via solution processing. *Light: Sci Appl* 2017; **6**: e17094.
- 56 Chen YH, Ma DG, Sun HD, Chen JS, Guo QX *et al.* Organic semiconductor heterojunctions: electrode-independent charge injectors for high-performance organic light-emitting diodes. *Light: Sci Appl* 2016; **5**: e16042.
- 57 Zou JY, Li CZ, Chang CY, Yip HL, Jen AK. Interfacial engineering of ultrathin metal film transparent electrode for flexible organic photovoltaic cells. *Adv Mater* 2014; **26**: 3618-3623.
- 58 Kang H, Jung S, Jeong S, Kim G, Lee K. Polymer-metal hybrid transparent electrodes for flexible electronics. *Nat Commun* 2015; **6**: 6503.
- 59 Bi YG, Feng J, Ji JH, Chen Y, Liu YS *et al.* Ultrathin and ultrasmooth Au films as transparent electrodes in ITO-free organic light-emitting devices. *Nanoscale* 2016; **8**: 10010-10015.
- 60 Zhong GY, Liu Y, Song J, Zhao Q, Li YS *et al.* Strong piezoresistance effect of small molecule organic semiconductors. *J Phys D: Appl Phys* 2008; **41**: 205106.
- 61 Kim JH, Seo SM, Lee HH. Nanovoid nature and compression effects in organic light emitting diode. *Appl Phys Lett* 2007; **90**: 143521.

- 62 Schulz P, Cowan SR, Guan ZL, Garcia A, Olson DC *et al.* NiO_x/MoO₃Bi-layers as efficient hole extraction contacts in organic solar cells. *Adv Funct Mater* 2014; **24**: 701-706.
- 63 Rafique S, Abdullah SM, Shahid MM, Ansari MO, Sulaiman K. Significantly improved photovoltaic performance in polymer bulk heterojunction solar cells with graphene oxide/PEDOT: PSS double decked hole transport layer. *Sci Rep* 2017; **7**: 39555.

Figure 1 Schematic diagram showing the fabrication process for the stretchable electronic devices. (a) Depositing Al film on an elastomeric substrate by thermal evaporation via a metal stencil. (b) Removing the metal stencil from the elastomeric substrate. (c) Pre-stretching the elastomeric substrate. (d) Attaching an ultrathin electronic device onto the elastomeric substrate. (e) Releasing the pre-strained substrate to form stretchable electronic devices. (f) and (g) SEM images of the periodic Al film deposited onto the elastomeric substrate before and after stretching corresponding to (b) and (c), respectively. Insets show enlarged SEM images for the periodic Al film deposited onto the elastomeric substrate before and after stretching.

Figure 2 Demonstration of SOLEDs. SEM images (a) and photographs (b) of the SOLEDs at 0%, 50% and 100% tensile strain, respectively.

Figure 3 Photographs of the SOLEDs in a dark environment. (a) A large-area SOLED at 0%, 50% and 100% tensile strain. (b) An array of five OLED pixels at 0%, 50% and 100% tensile strain.

Figure 4 EL performance of SOLEDs. Current density-luminance-voltage characteristic curves (a) and current efficiency-voltage characteristic curves (b) for the SOLEDs. Device performance under a cyclic stretching test between 0% and 20% strain (c) and between 0% and 60% strain (d).

Figure 5 Characterization of SPSCs. (a) J-V characteristic curve for a planar polymer solar cell. (b) J-V characteristic curves for the SPSCs at different strain values. (c) Parameters for the SPSCs at different strain values. (d) Device performance under a cyclic stretching test between 0% and 20% strain.









